

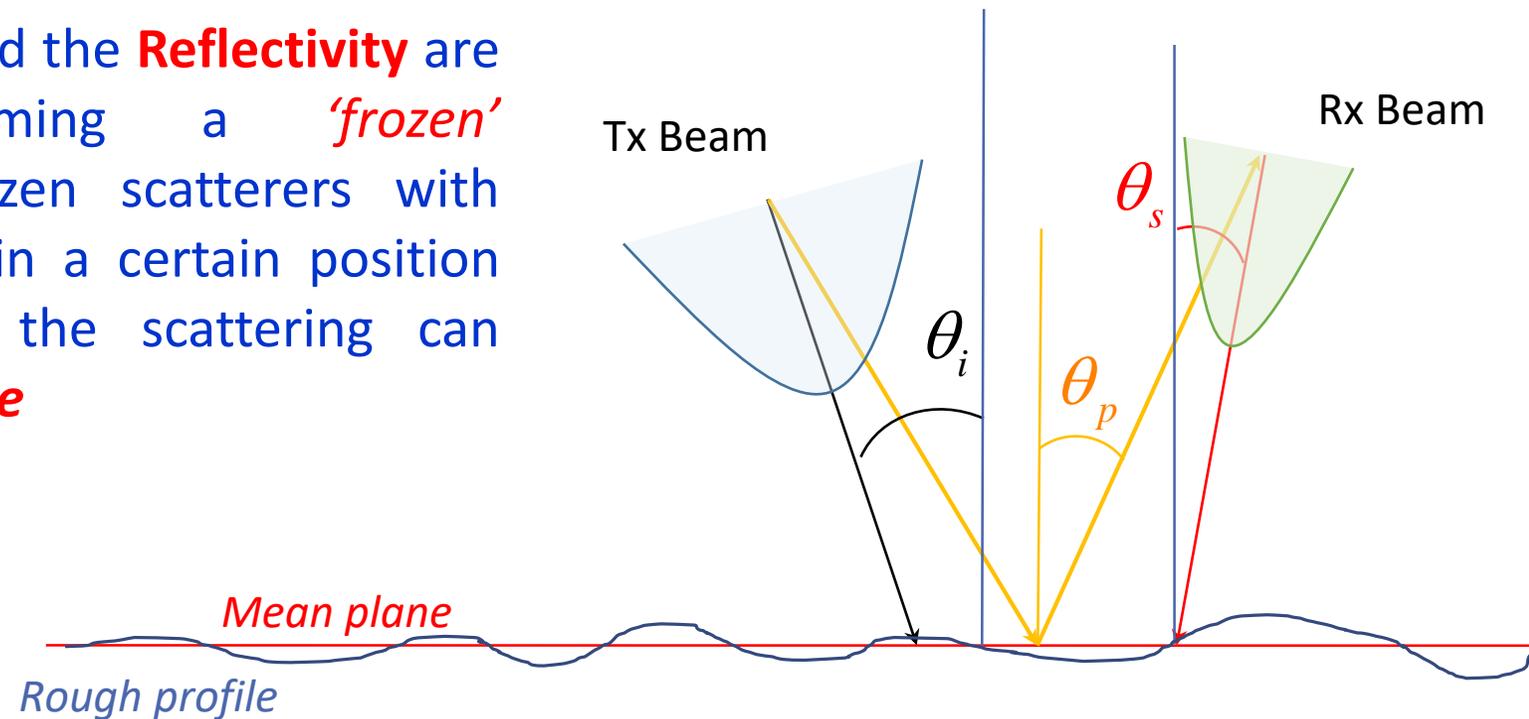


Spatial Coherence of GNSS-R Signals: A Numerical Investigation

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- ✓ The scattered field is generated by the superimposition of an *incoherent* and a *coherent* field
- ✓ The two contributions are generally represented by the *Normalized Radar Cross Section (NRCS)* and the *Surface Reflectivity*
- ✓ However if the *NRCS* and the *Reflectivity* are achieved by assuming a *'frozen' configuration*, i.e., frozen scatterers with both antennas placed in a certain position over the 2-D space, the scattering can present *phase coherence*

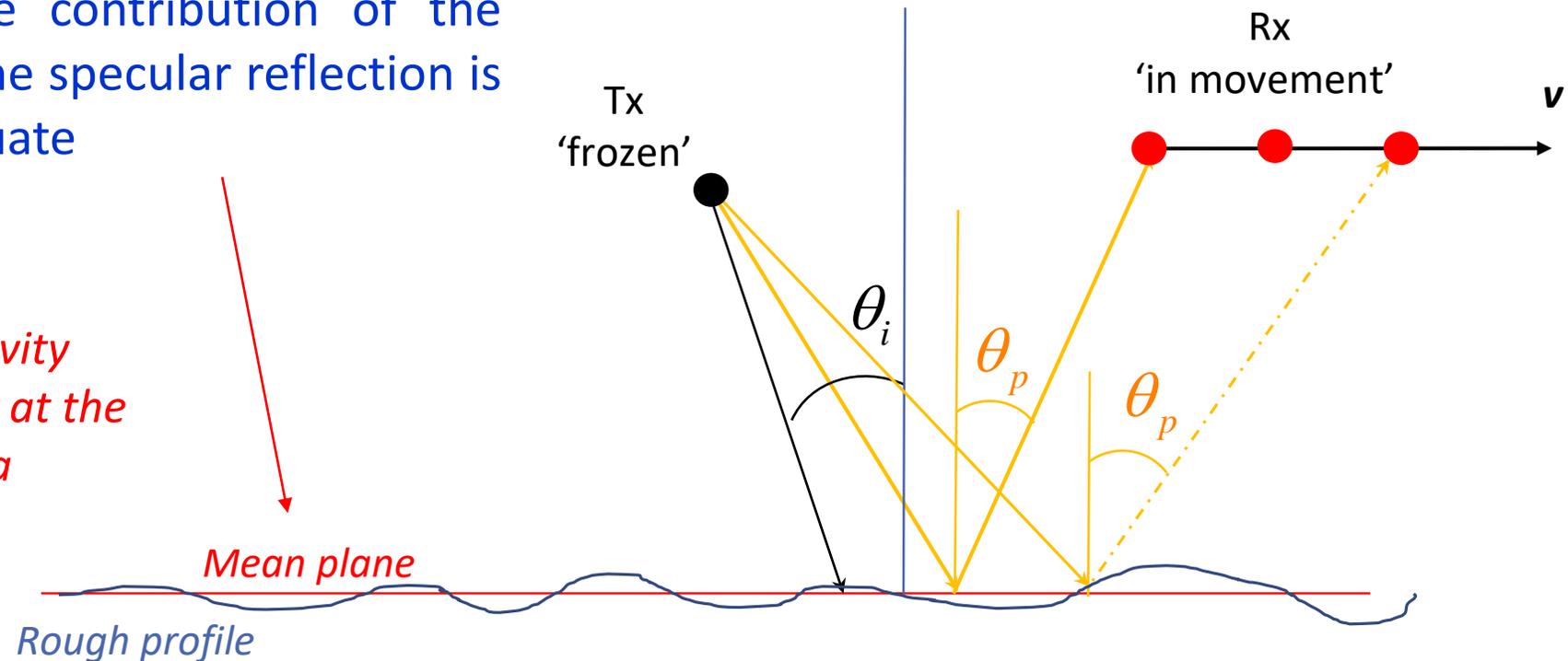


✓ The **relative movements** of transmitter and receiver and the system resolution, combined with the random nature of the illuminated surface, affect the **coherence** of the **scattered field**

✓ For a flat surface, the **coherent component** is, by definition, the contribution of the **'mean plane'**. Thus, the specular reflection is expected not to fluctuate



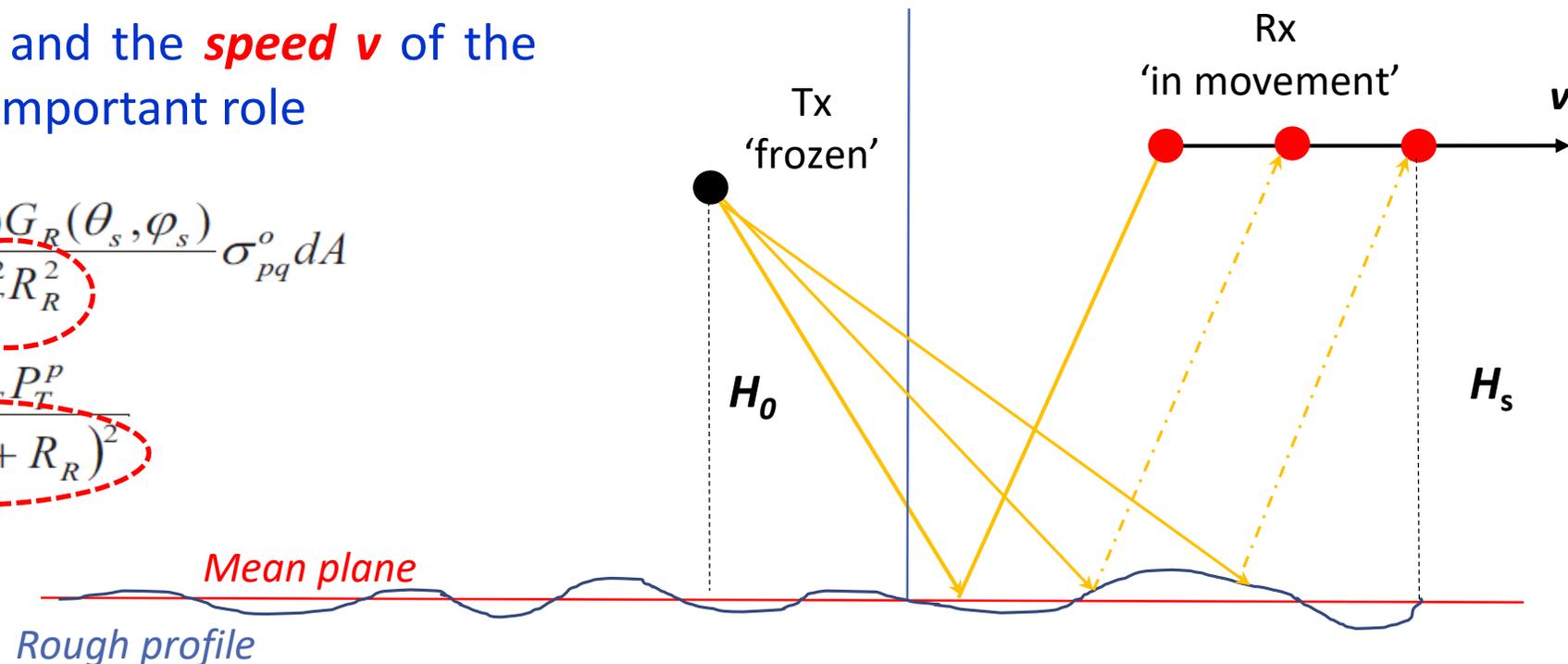
The surface reflectivity determines the power at the receiver antenna



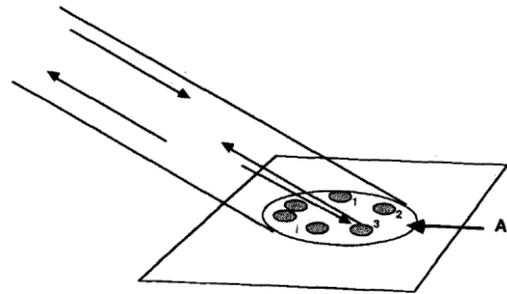
- ✓ A change in **coherence** can have a detrimental effect on the coherent and incoherent **integration** of the radar echoes at the receiver
- ✓ **Long term fluctuations** would not be mitigated by incoherent integration (fewer independent samples)
- ✓ Both the **height** and the **speed v** of the receiver play an important role

$$P_r^{q(incoh)} = \frac{P_T^p \lambda^2}{(4\pi)^3} \int \frac{G_T(\theta_i, \varphi_i) G_R(\theta_s, \varphi_s)}{R_T^2 R_R^2} \sigma_{pq}^o dA$$

$$P_r^{q(coh)} = \Gamma_{pq} \frac{\lambda^2 G_T G_R P_T^p}{(4\pi)^2 (R_T + R_R)^2}$$



- ✓ In the literature, the **spatial coherence** has mainly been characterized in the frame of SAR interferometry considering backscattering



Uncorrelated scatterers within the resolution cell

Li, Fuk K. and Richard M. Goldstein, "Studies of multibaseline spaceborne interferometric synthetic aperture radars." *IEEE TGRS* 28.1 (1990): 88-97.

Zebker, Howard A. and John Villasenor, "Decorrelation in interferometric radar echoes." *IEEE TGRS*, 30.5 (1992): 950-959.



Simple expression provided for the correlation as a function of the **system baseline** assuming a 2-D distribution of **uncorrelated scatterers**

- ✓ The effect of the local terrain slope was accounted for by *Franceschetti et. al.*, later in the frame of the Kirckhoff scattering theory

Franceschetti, G., et al. "The effect of surface scattering on IFSAR baseline decorrelation." *JEWA* 11.3 (1997): 353-370.

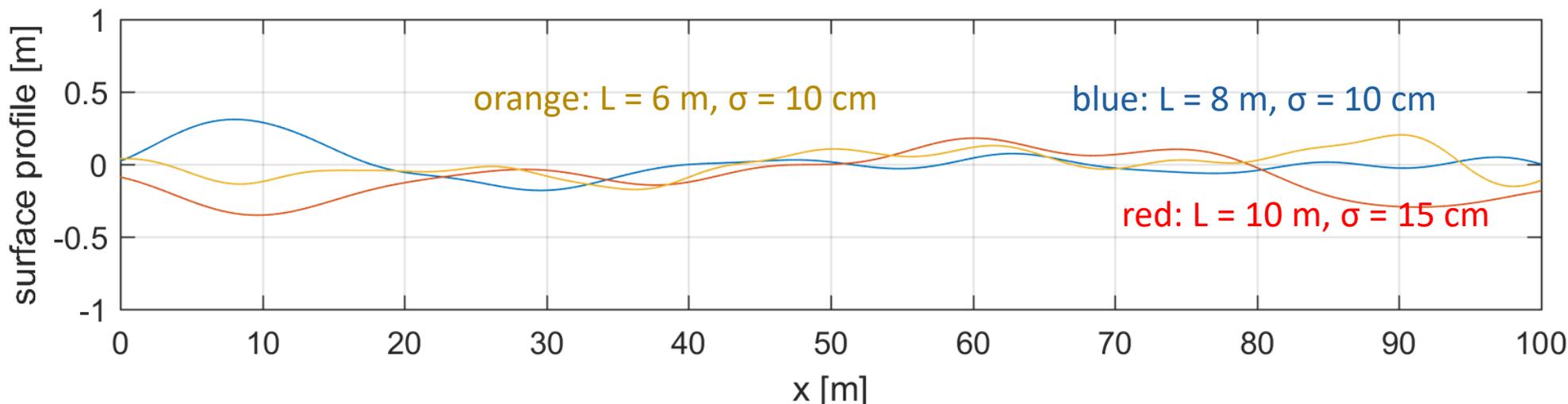
- ✓ Over a very flat area one would not expect fluctuations from satellite height, as diffuse component is greatly attenuated (due to free space losses)
- ✓ Instead fluctuations can be very high, larger than from an airborne receiver (Disomogeneity? Instrument? others?)

- ✓ The question is: a «flat area» is really flat?
- ✓ What about the presence of water bodies?

✓ Gentle undulations may occur at large scale, i.e., low height (~5-15 cm) and long correlation length (~6-10 m)

✓ Validity limits scalar KA almost always ok for a general assessment:

$$(qz * \sigma)^2 \gg 10 \quad k_0 * \sigma \gg 2$$



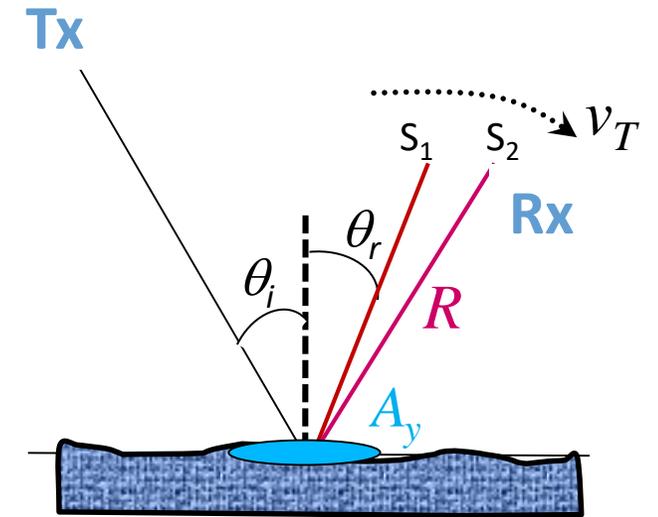
Surface profile over 100 m

- ✓ For an *incoherent* scattering the signal fluctuates (speckle “noise”).

- ✓ When Rx moves from S1 to S2, if the *target* A_y consists of *uniformly distributed uncorrelated scattering centers*, the *decorrelation time* (see e.g., Zuffada et al., 2003, RSoEnv, Zebcker, 1992, TGRS) is given by

$$T_C = \frac{\lambda R}{2v_T A_y \cos^2 \theta_i}$$

for a plane 100 m high, $v_T = 60$ m/sec, 15° incidence, $T_C = 2.4$ msec

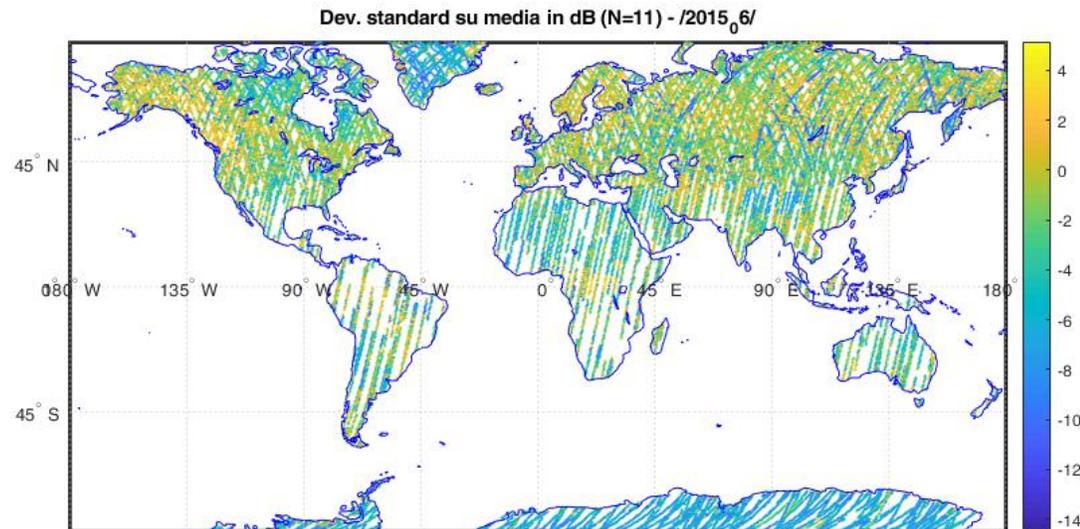
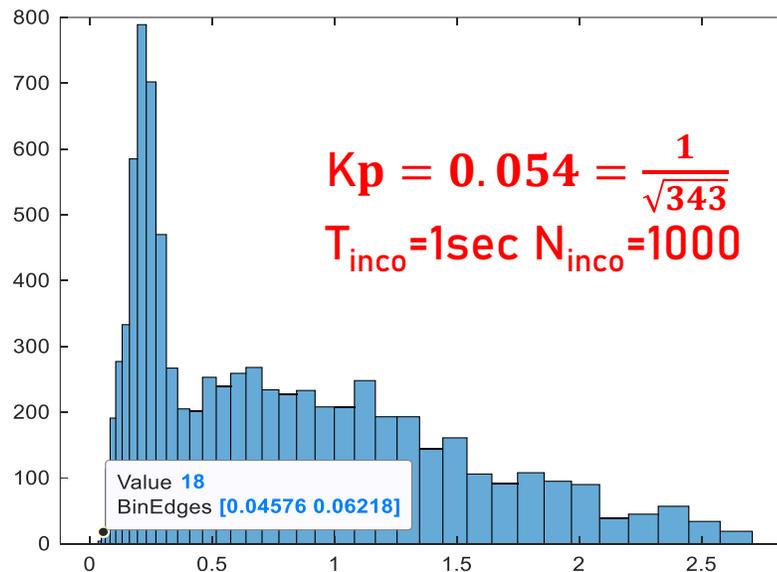


- ✓ **How the coherent signal is expected to fluctuate?**

Limit case: the variability determined by a *pure coherent reflection* from a flat infinite surface should be zero

- ✓ The presence of water bodies is expected to generate coherent signals...

Histogram of *the coefficient of variation* ($K_p = \text{std}/\text{mean}$) of TDS reflectivity within 11 samples, i.e., over 11 secs (70 km).



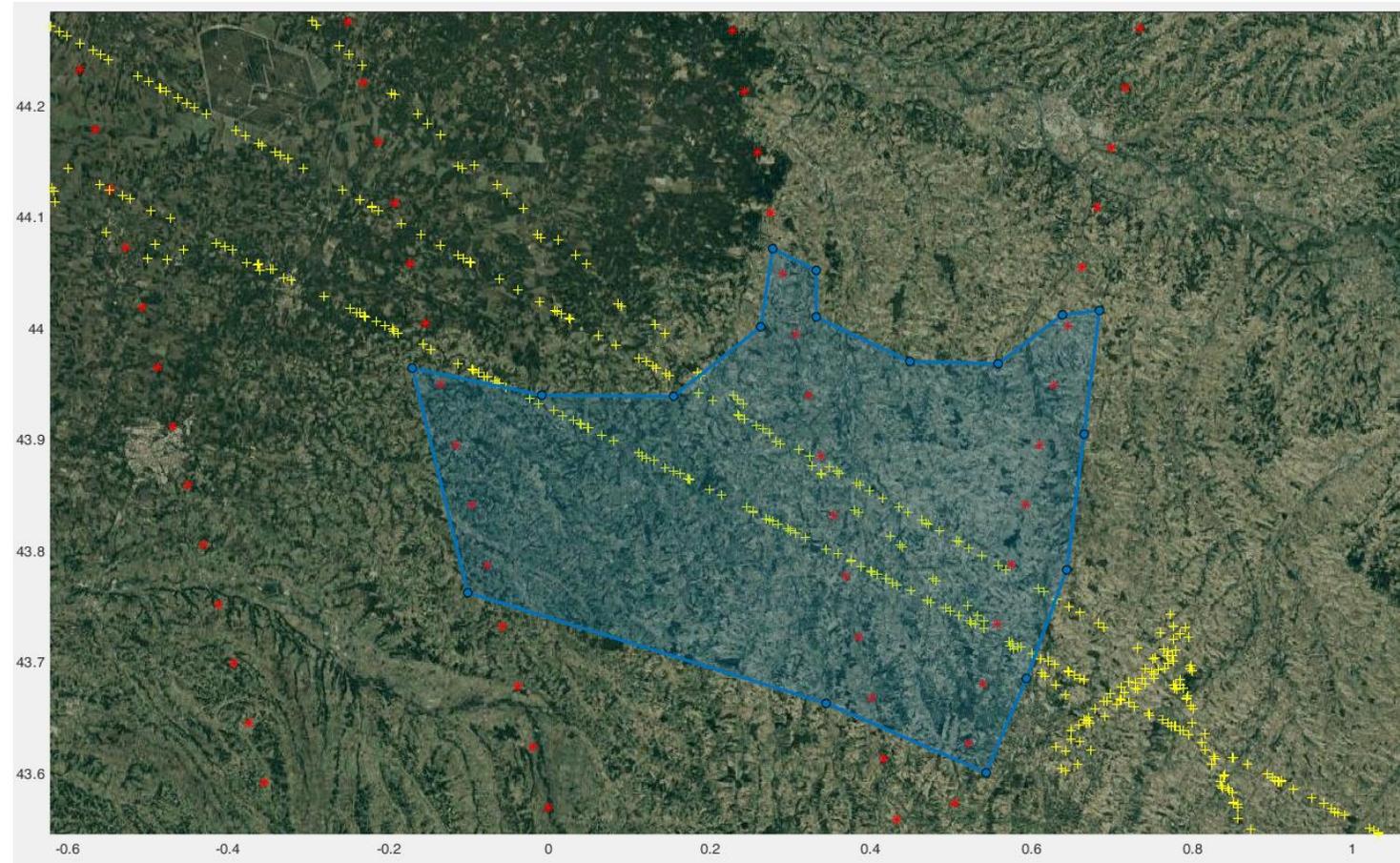
Most homogenous areas is Antarctica

- Minimum value (i.e., mostly homogenous areas) ~ 0.05 . **In Antarctica the scattering should not be assumed completely coherent**
- It corresponds to **340 looks** ($k_p = 1/\sqrt{340} = 0.054$) as compared to 1000 samples average (1 sec incoherent, 1 msec coherent integration). **Therefore, as expected, there is a certain degree of correlation between samples...**

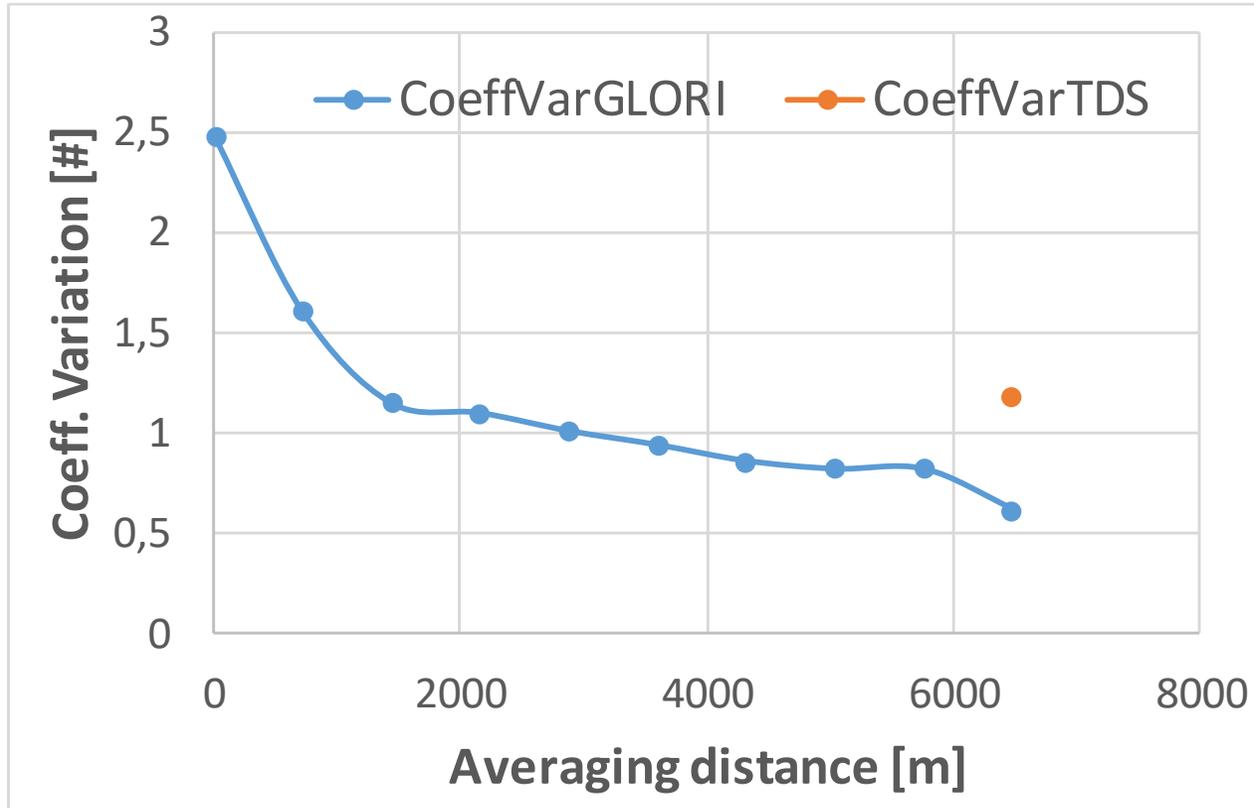
TDS-1 data (red, 1 ms coherent) at 1 sec (incoh, 6.5 km distance made) and GLORI data (yellow, 20 ms coherent) averaged incoherently over different distances (from 15 m to 6.5 km) were analysed on a common quite homogeneous agricultural area

GLORI data: kindly provided by Dr. Zribi (CESBIO), in the frame of an ESA project.

Thanks!!



Coefficient of variation



GLORI:

$$T = \frac{\text{space}}{\text{velocity}} = \frac{6.5 \text{ km}}{60 \text{ m/sec}} = 108 \text{ sec}$$

$$N_c = \frac{\text{time span}}{T_{\text{coheren}}} = \frac{108 \text{ sec}}{20 \text{ msec}} = 5400 \text{ samples}$$

TDS:

$$N_c = \frac{1 \text{ sec}}{1 \text{ msec}} = 1000 \text{ samples}$$

- ✓ Kp not zero, the scattering should not be considered fully coherent
- ✓ Integrating more samples with GLORI, Kp gets smaller...

- ✓ Both the Spaceborne and the Airborne case generally suggest the scattering cannot be fully coherent, neither incoherent....

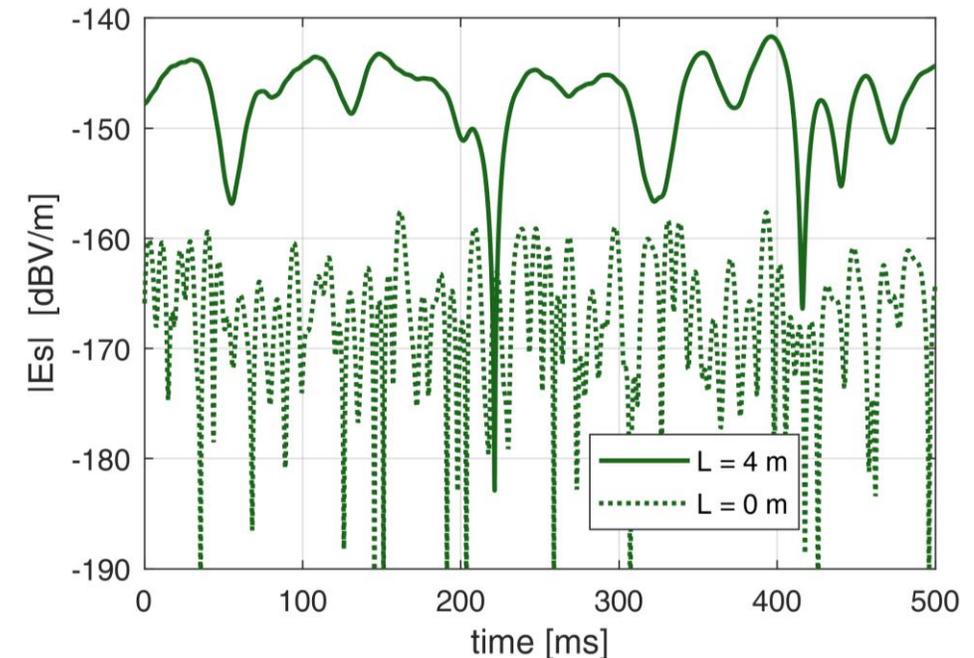


- ✓ Simulation of 2-D Gaussian surfaces with different correlation lengths: $H=100$ m, $v=60$ m/sec, 15° beam
- ✓ Kirchhoff scalar solution versus time/position for a moving RX

Full-wave numerical solution of the KA integral including Sphericity and Antennas Gains:

$$E_s = -\frac{jk_0 a_0}{4\pi} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \frac{e^{-jk_0(R_1+R_2)}}{R_1 R_2} e^{-g_0^2(\cos^2 \theta_0 x^2 + y^2) - g_s^2(\cos^2 \theta_s x^2 + y^2)} dx dy$$

E-field versus time/position for $\sigma = 6$ cm (rms h.)



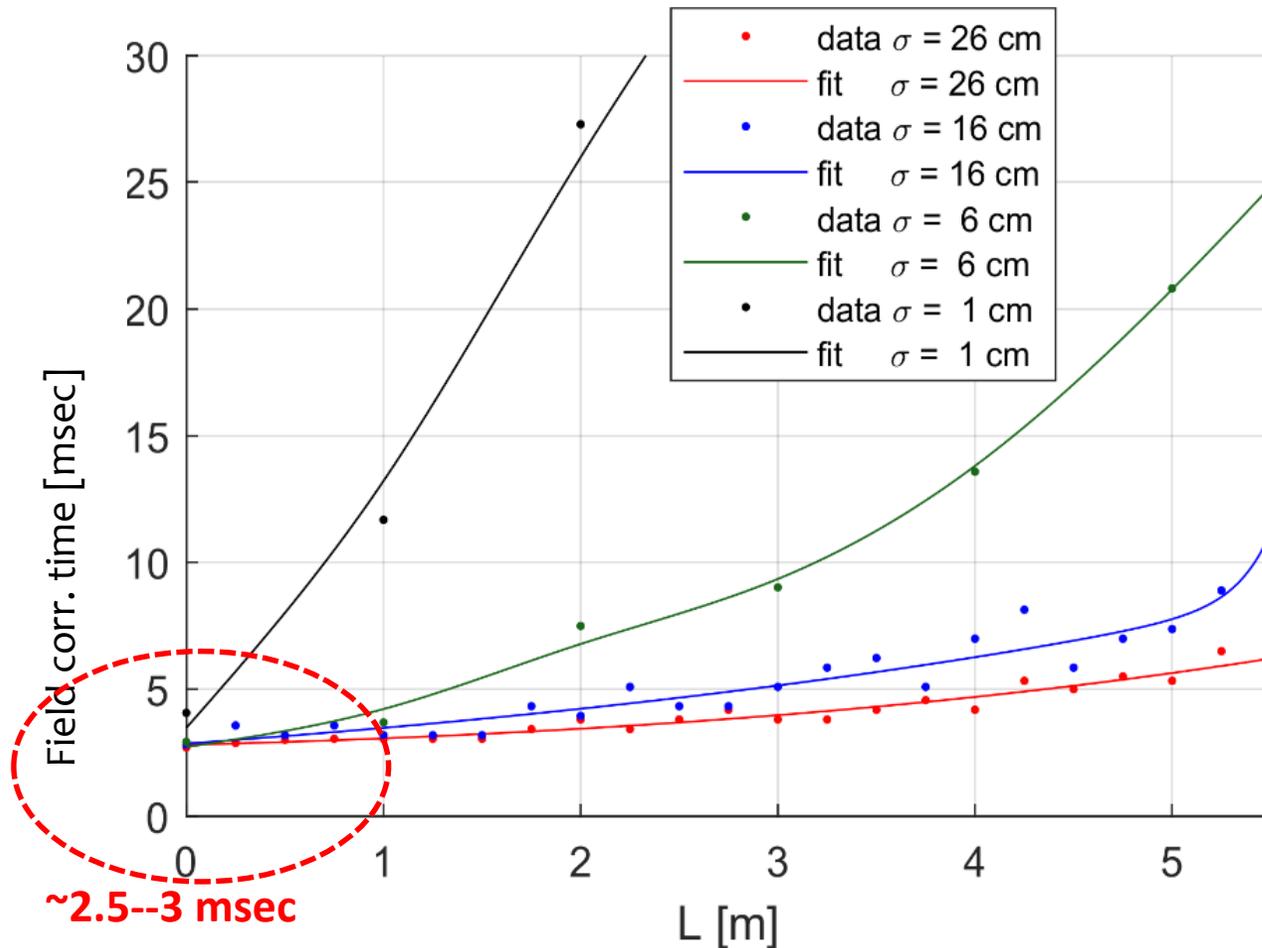
Strong dependence of the E-field profiles on $L...$



✓ $H=100$ m, $v=60$ m/sec, 15° beam

Coherence time evaluated as:

$$\tau \text{ so that } \langle E_s(t+\tau)E_s^*(t) \rangle / \langle |E_s(t)|^2 \rangle = 1/e$$



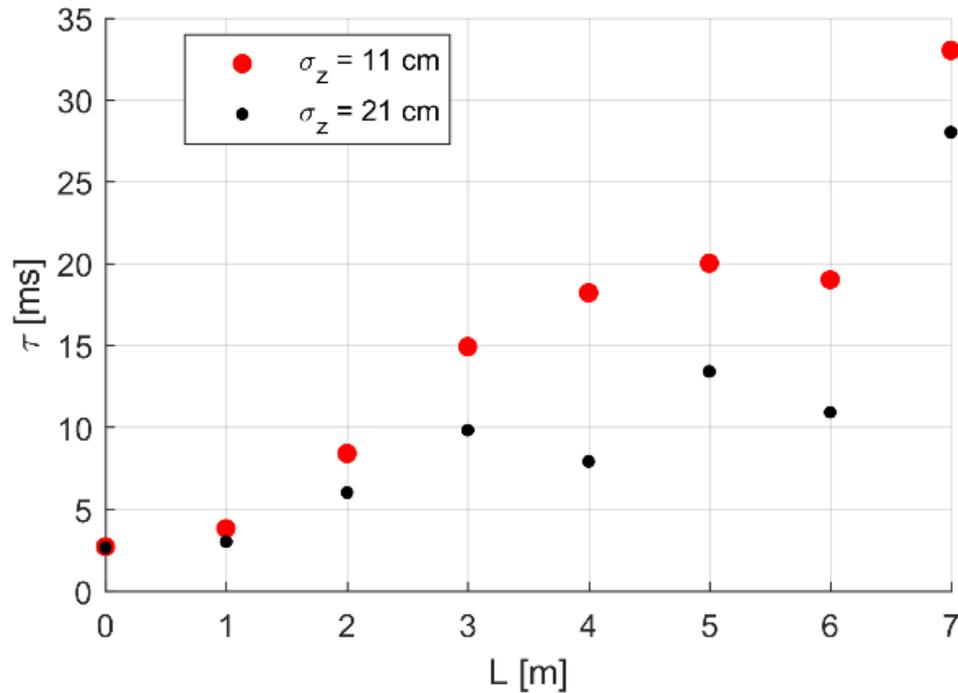
✓ The correlation **increases** with L , **decreases** with σ

✓ Curves fitted with exponential functions

✓ Values achieved for L tending to zero in agreement with theory

Numerical solution for higher receiver but same speed

$H = 200$ m, $v = 60$ m/sec, 15° beam



Note: Antennas area directed along the specular point

✓ Increasing the receiver height, **larger coherence time** can be expected, but the speed also generally increases...

✓ As is visible, larger **rms heights** are responsible for a reduction of the **coherence time**



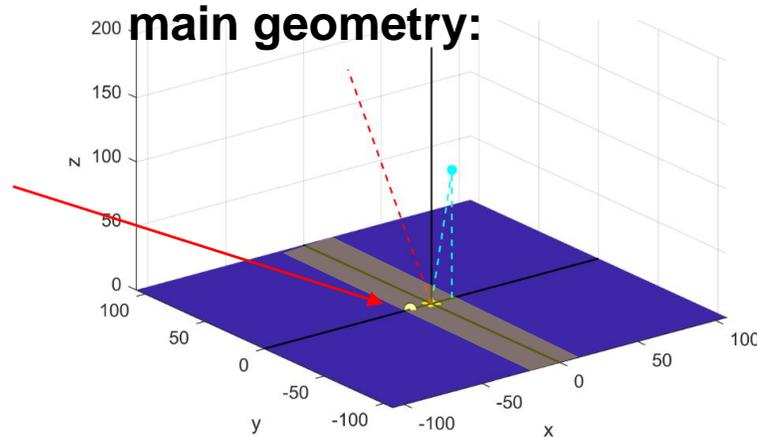
The field coherence is strongly related to both L and the surface σ (rms h).

Note: to limit the computation time we consider here just one surface realization (Frequency averaging and/or Monte Carlo are in progress...)

- ✓ Yellow: flat PEC
- ✓ Blue dielectric with $\epsilon_r = 4$ (flat or rough)

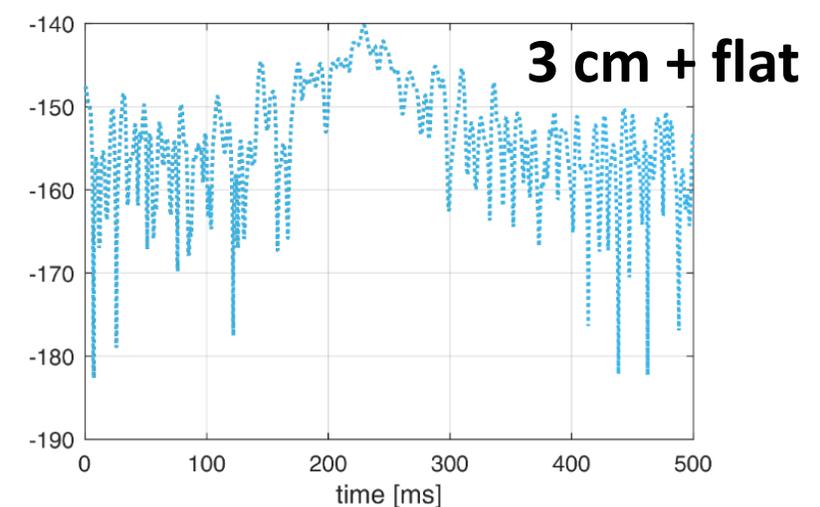
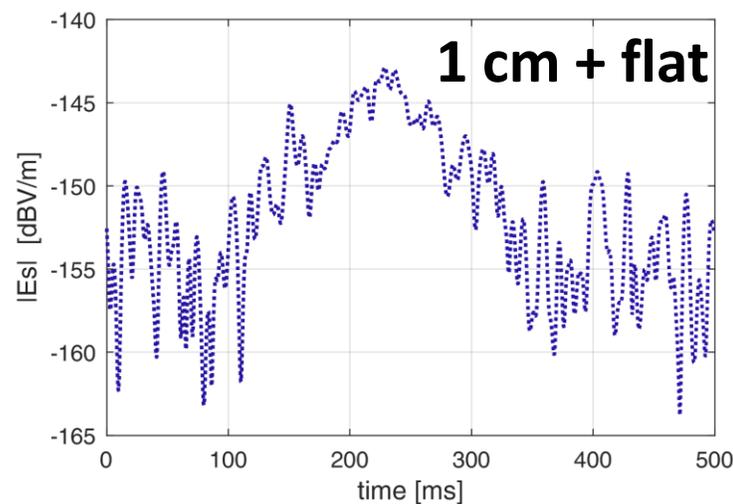
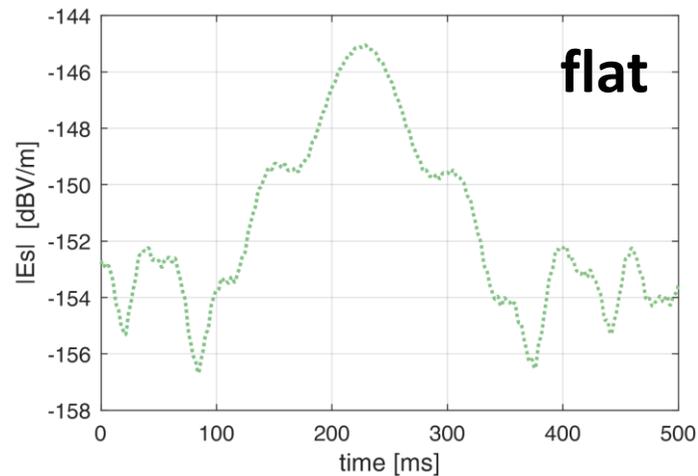
Tx, Rx beams = $45^\circ, 67^\circ$;
Rx = 100 m, Tx = 20 000 km

Rx -3B footprint = 100 m
PEC side 10 m
(comparable with FFz)

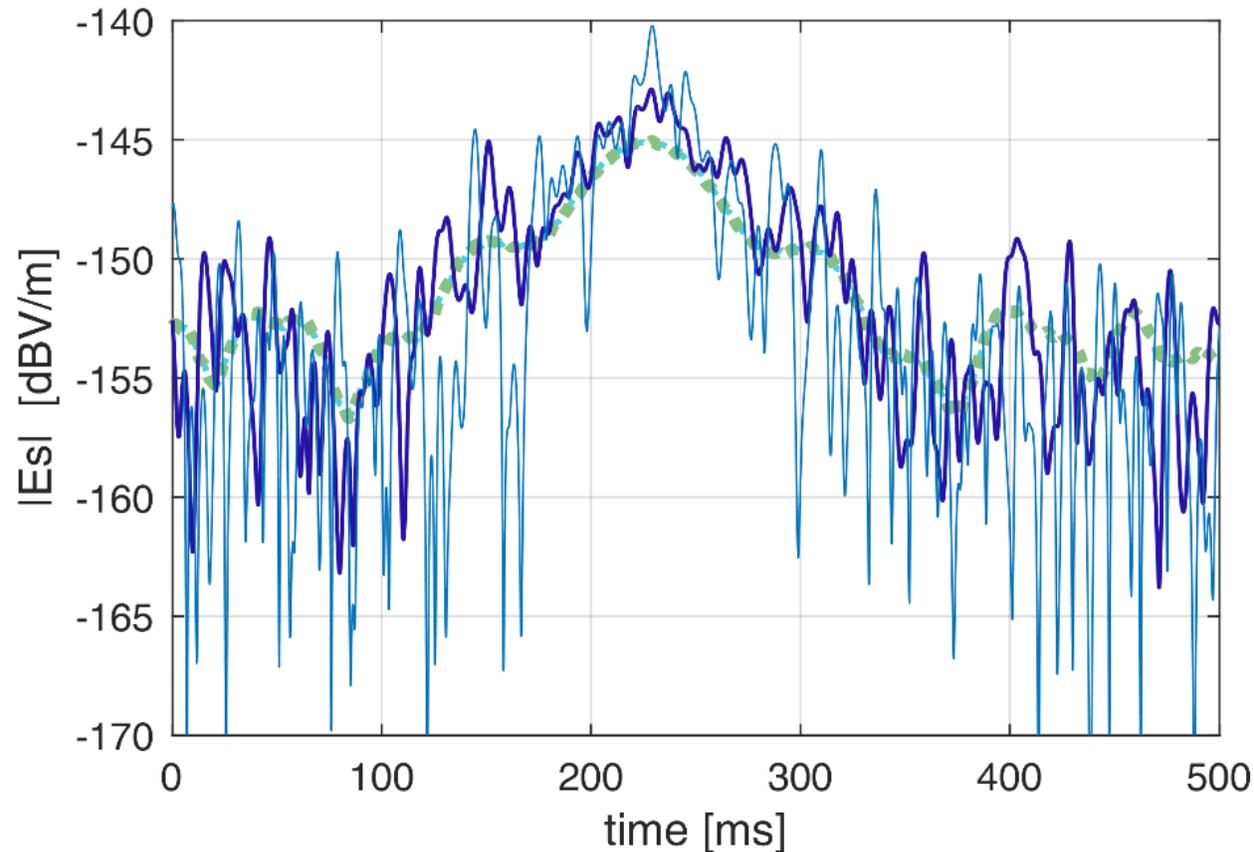


Starting position of the specular point

- ✓ Electric field versus time|position for an airborne Rx
- ✓ Transition through boundary is progressive with oscillations due to Fresnel zone interferences.
- ✓ When relatively small water bodies are considered, Fresnel oscillations can be masked in case of rough surfaces

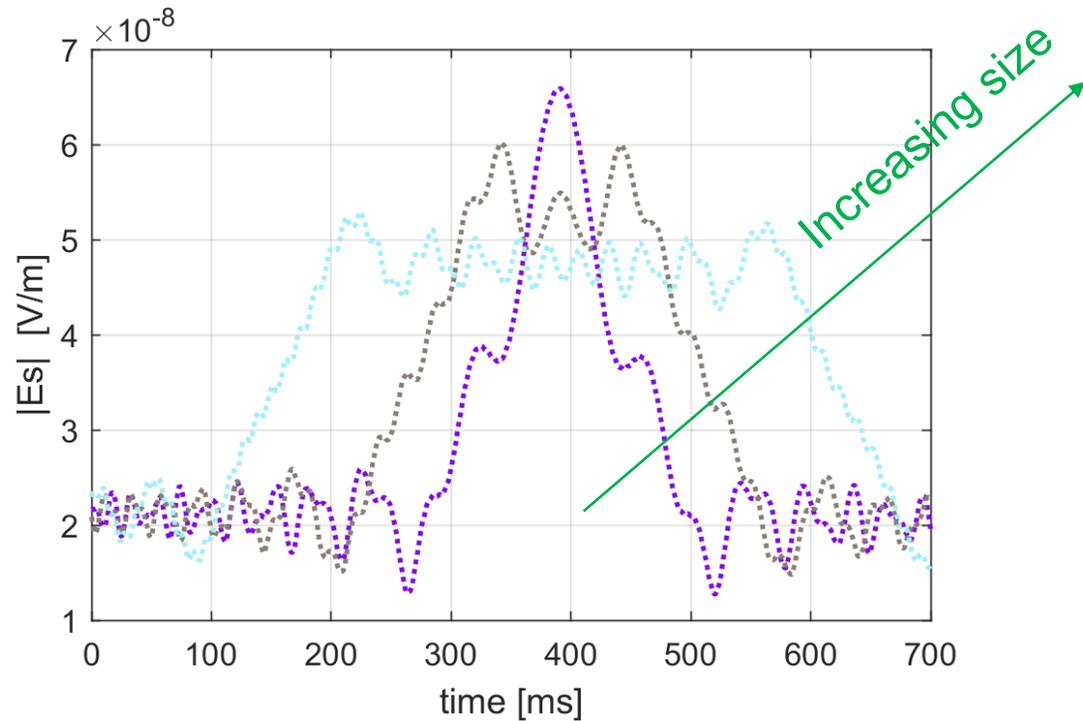


Comparison over the same figure frame:

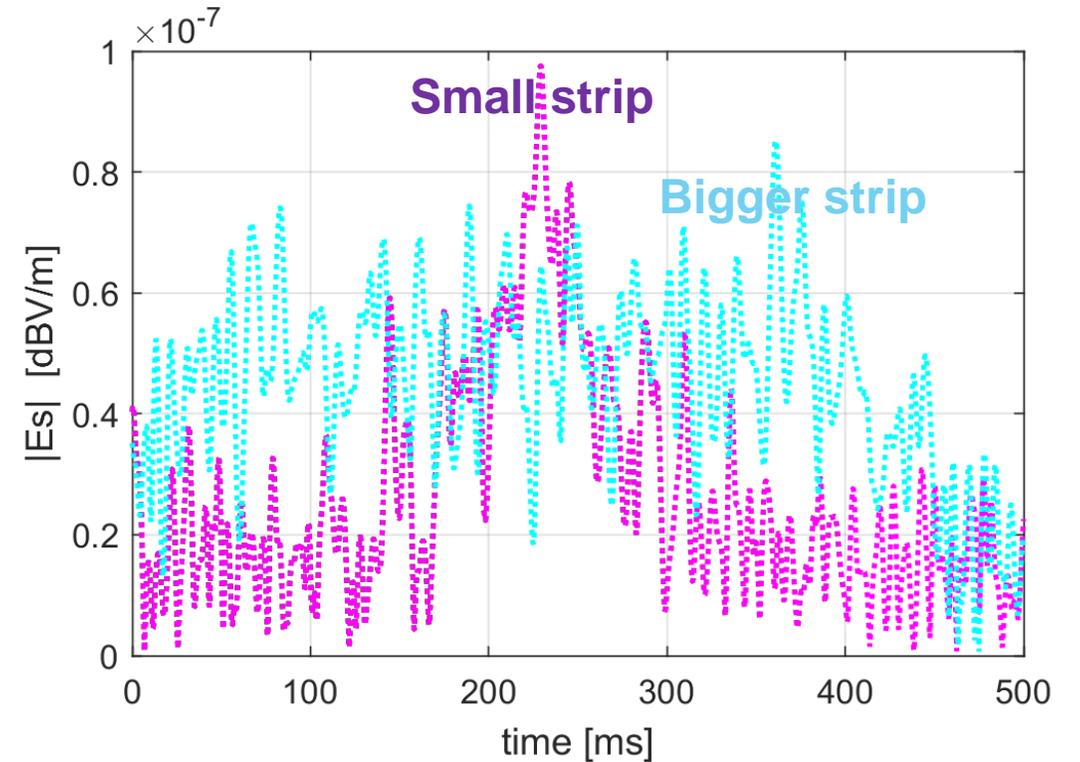


- ✓ Note: the field at the receiver is equal to 1 V/m
- ✓ The **statistical fluctuations** are superimposed to the gentle ones related to the **Fresnel oscillations** determined by the presence of a **clear reflector**, which can be potentially masked

✓ All the flat



✓ Flat + 3 cm



✓ As expected, changing the size the fluctuation patterns vary

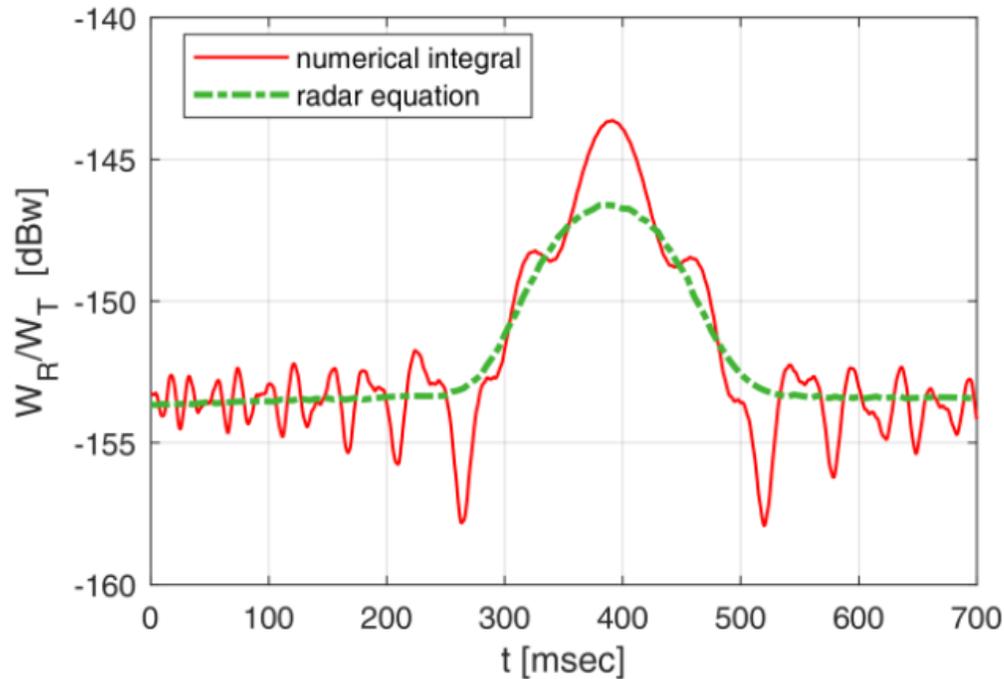
✓ The masking effect can be very strong in the presence of roughness

- ✓ To model the power at the receiver for the spaceborne case we developed an **approximate model** for the coherent scattering

- ✓ Based on the definition of a *'true'* NRCS associated to the coherent component

F. T. Ulaby, C. T. Allen, and A. K. Fung, "Method for retrieving the true backscattering coefficient from measurements with a real antenna," *IEEE Trans. Geosci. Remote Sens.*, vol. GE-21, no. 3, pp. 308-313, Jul. 1983.

- ✓ The solution is more convenient and allows for including both the ***incoherent*** and ***'coherent'*** scattering in the bistatic radar equation...



More details during the inLab Session...



- ✓ We have numerically analyzed the signal fluctuations with respect to the surface parameters
- ✓ 1msec (spaceborne) to 20msec (airborne) coherent integration do not filter out those fluctuations. Incoherent integration smooth them according to number of independent samples N_c ...
- ✓ We observed that the ***specular component*** (coherent in what extent?) ***fluctuates*** with long correlation time
- ✓ A significant dependence of the correlation time of L and σ has been observed...

Work in progress as regards the spaceborne configuration....
Useful information could be achieved to help selecting the incoherent integration time

Thanks!!



